

Oxidation-reduction equilibria of vanadium in CaO-SiO₂, CaO-Al₂O₃-SiO₂ and CaO-MgO-SiO₂ melts

H. FARAH ^{*,†}

Department of Mechanical and Industrial Engineering, Concordia University, Montreal, QC H3G 1M8, Canada

E-mail: farah_1@me.concordia.ca

M. BRUNGS

School of Chemical Engineering and Industrial Chemistry, University of New South Wales, Sydney 2052, Australia

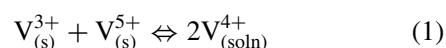
A series of redox studies of vanadium have been carried out in CaO-SiO₂, CaO-MgO-SiO₂ and CaO-Al₂O₃-SiO₂ melts/slugs equilibrated over oxygen partial pressures (pO₂) range 10⁻²–10⁻⁹ atm at 1600°C. V₂O₅ level was varied from 1–5 mol%. Three different melt basicities and alumina contents were investigated. Magnesia content was varied between 3.5 and 4.9 wt%. A newly developed analytical technique based upon electron paramagnetic resonance (EPR) spectroscopy was successfully applied to these melts. Two redox equilibria corresponding to V³⁺/V⁴⁺ and V⁴⁺/V⁵⁺ pairs followed the O-type redox reaction over the oxygen partial pressure range investigated. Higher oxidation states of vanadium were stabilized with increasing basicity of slags. Two redox pairs coexisted within oxygen pressure region 10⁻⁴–10⁻⁶ atm. However, redox ratios did not indicate clear trends with increasing V₂O₅ content in CaO-SiO₂-V₂O₅ system. In CaO-SiO₂-Al₂O₃-V₂O₅ slags, a slight increase in redox ratios (V³⁺/V⁴⁺) was obvious when alumina quantity was changed from 3.22 to 5.44% at a basicity ratio ~1.3, indicating an increase in slag acidity. CaO-MgO-SiO₂-V₂O₅ slags showed a sharp decrease in redox ratios (V⁴⁺/V⁵⁺) between 10⁻²–10⁻⁶ atm with addition of 3.5 wt% MgO, due to increasing free oxygen ions in slags.

© 2003 Kluwer Academic Publishers

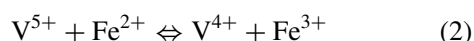
1. Introduction

In our previous study [1, 2], vanadium redox equilibrium has been described in quenched sodium silicates. However the fundamental redox data of vanadium in iron free and iron bearing calcium silicates is unavailable and/or limited. As stated earlier in our work [1–3], vanadium redox chemistry is not yet completely understood because of the existence of the multiple oxidation states. Previous work [4–6] has indicated that one of the major difficulties in interpretation of the vanadium redox reaction in melts is the dependence on conventional analysis, which seriously affects the accuracy of the results. Vanadium can exist either as V³⁺/V⁴⁺ or V⁴⁺/V⁵⁺ redox pair depending on slag composition, although it is possible that over a certain range of oxygen potential, they could coexist at the experimental temperature in these slags. When this occurs, determination of various vanadium species via analysis in aqueous solution presents difficulties in that the following

reaction occurs:



In addition, the iron in the slags could interfere with vanadium analysis by the following reaction [7, 8]:



Thus before wet chemical analysis, it is essential to determine accurately the concentration of at least one of vanadium species to enable wet chemical results to be corrected for reaction 1 or 2. The details have been discussed in our work elsewhere [1–3, 9, 10].

Mittelstadt and Schwerdtfeger [4] studied calcium silicates with different basicity ratios at 1600°C over a range of pO₂ (10⁻¹–10⁻⁸ atm) and 10 mol% V₂O₅ content. However vanadium volatilization was reported under reduced oxygen pressures, which was compensated by reoxidising the sample after equilibration;

*Corresponding address: C.P. 47527, 1550 de Maisonneuve West Montreal, QC H3G 2V7, Canada.

†Humera Farah and Michael Brungs are faculty members at their respective departments.

nevertheless this approach could have affected the accuracy of the results. The authors commented that the three vanadium valencies couldn't be analysed in aqueous solution together, owing to the reaction (1).

The CaO-MgO-FeO_x-SiO₂ steelmaking slags studied by Inoue and Suito [11] were equilibrated with liquid iron at 1550–1650°C and were then chemically analysed in aqueous solution, assuming that the Fe³⁺/Fe²⁺ ratio is same in these slags, as in the slags without vanadium at a fixed composition. These factors contributed to the error in determination of the true valency of vanadium. The author also admits that the assumption, that only two vanadium species can coexist, could affect the actual vanadium valency. Vanadium distribution between the slag and metal increased as the CaO/SiO₂ ratio was raised, as expected.

Fig. 1 presents a comparison of the valency ratios (V⁴⁺/V⁵⁺) versus (CaO + MgO)/SiO₂ molar ratios at different temperatures (1550–1650°C) using tabulated data from Inoue and Suito's work. The presence of the V⁴⁺/V⁵⁺ pair at this reduced pressure disagrees with that of Mittelstadt and Schwerdtfeger [4] who determined an overall valance of 1.8, corresponding to a (V³⁺/V⁴⁺) redox pair under oxygen potential ≤ 10⁻⁸ atm. However Inoue and Suito admit that it is possible that iron free CaO-SiO₂ slag would contain V³⁺ ion at this oxygen pressure since V³⁺ ion is evident at 10⁻⁸–10⁻⁹ atm in V-O system. Therefore it is likely that iron has affected the true vanadium valency in these slags. An effect of increasing temperature on the redox ratios is also not evident.

While determining the phosphorous distribution between magnesia saturated steelmaking slag (CaO-MgO-FeO_x-SiO₂) and liquid iron at 1600°C, Selin [12, 13] found the overall composition of the melt corresponded to oxidation state V⁴⁺. Since the vanadium valance states were not determined, this finding cannot indicate the true redox pair of vanadium present at the reduced oxygen partial pressure.

In another study made by Tsukihashi *et al.* [5], vanadium valencies were measured in CaO-CaF₂-Na₂O-SiO₂ at 1300°C. V⁴⁺ and V⁵⁺ ions were found dominant in these slags and the valency increased with an increase in sodium oxide content from 0–3 wt%. Werme and Astron [14–16] studied the fundamentals of the vanadium redox ions during the distribution experiments between carbon saturated iron and CaO-Na₂O-SiO₂ (TiO₂, Al₂O₃, MgO) and FeO(satd)-SiO₂ slags at 1300°C with ~1.7% vanadium. Vanadium was found as monomer V³⁺ and VO⁺ ions in silica saturated slags and as VO₂⁻ ion in FeO rich slags. Since wet chemical analysis was used, the prediction of the true vanadium valency was affected and in addition the iron in the slags could have interfered with the vanadium analysis.

Contradictory behavior regarding the vanadium distribution was also reported by Werme [14, 15] when he examined the addition of CaO, MgO, Na₂O, Al₂O₃ and TiO₂, to iron and silica saturated FeO-SiO₂ melts and found that distribution ratio of vanadium between slag and iron decreased with increasing addition of CaO, MgO, Na₂O and Al₂O₃ under SiO₂ saturation, which is in contrast to his previous findings.

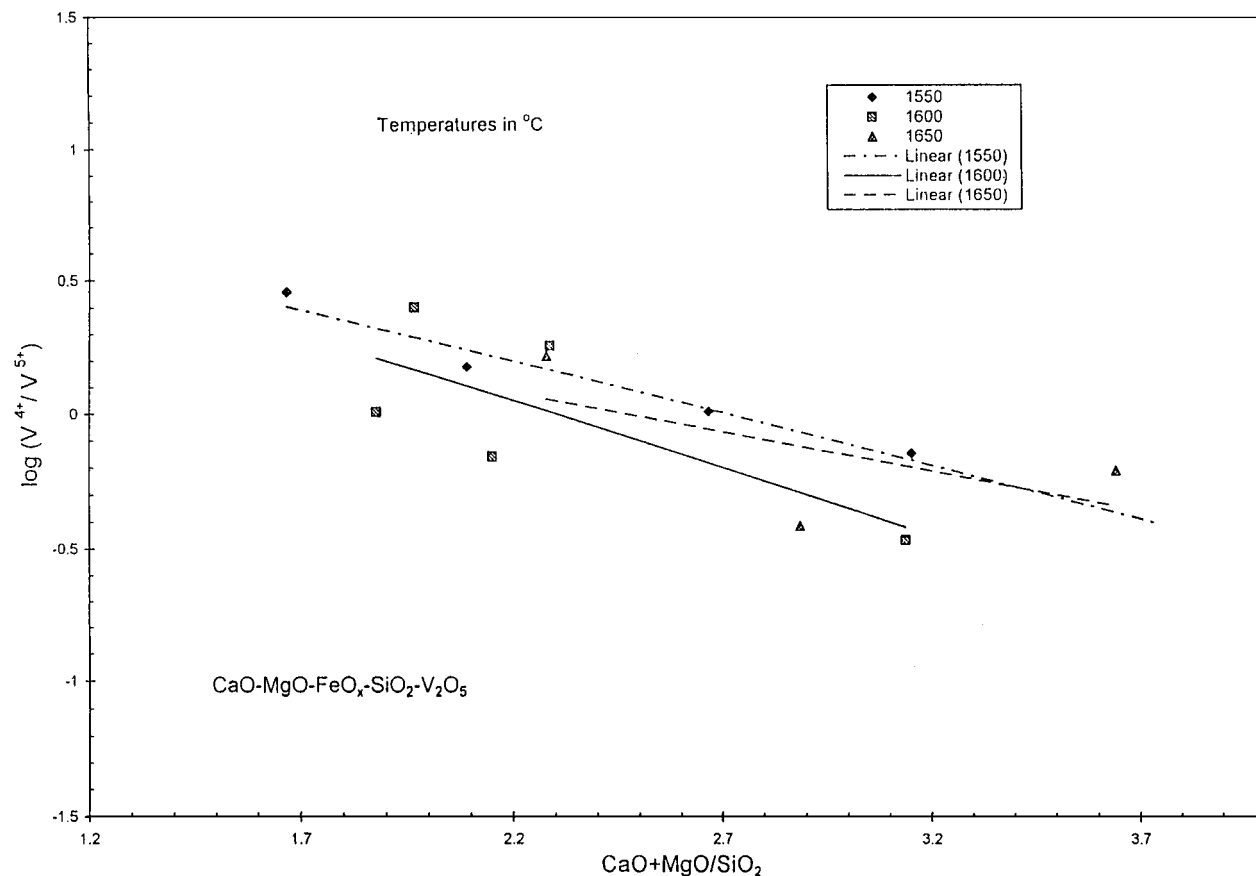
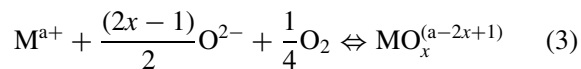


Figure 1 Variation of (V⁴⁺/V⁵⁺) ratios with (CaO + MgO)/SiO₂ molar ratios for CaO-MgO-FeO_x-SiO₂-V₂O₅ slags at 1550–1650°C, Tabulated data from Inoue & Suito [11].

Free oxygen ions (O^{2-}) present in the slag led to the concept of slag basicity, which can be defined based upon ionic theory, as the activity of the free oxygen ions, a_O^{2-} [17] assuming basic components produce O^{2-} ions while acid components consume them. Redox equilibrium of an element with multiple oxidation states upon introduction into a melt can be represented by a mass expression named an O-type reaction [4, 18–20].



for one electron change between the valencies, where x is the number of oxygen atoms associated with the oxidized redox ion in the melt to form an oxo-anion. This expression accounts for the activity of free oxygen ion, a_O^{2-} and describe the equilibria of the redox ions forming oxo ions e.g., CrO_4^{2-} , VO_3^- . A second type of redox expression named as a R-type redox reaction [19] has been used to describe the redox equilibria of a number of ions i.e., Co^{2+}/Co^{3+} , Mn^{2+}/Mn^{3+} . The practical difference between O and R-type redox expressions is that they predict the opposite effect of melt basicity upon the concentration redox ratio [21]. That is, from expression 3, an increase in melt basicity moves the equilibrium in favour of formation of the lower oxidation state, whereas the opposite effect is predicted by R-type reaction. Wright and Jahanshahi [19] reviewed the vanadium redox behavior in various melts and concluded that the vanadium follows an O-type redox reaction. However in some studies, either or both O and R-type equations have been used to describe the vanadium redox reaction, which is misleading and contradictory [4, 6, 11, 24].

In previous studies, the redox data of vanadium is mostly generated using chemical analysis and is available over a limited range of oxygen potential, temperature and melt composition. The aim of this present work was to utilize the newly developed analytical technique based on Electron Paramagnetic Resonance spectroscopy (EPR) in order to remove: (1) one of the major difficulties in interpretation of the vanadium redox reaction, that is dependence on conventional analysis, which often seriously affects the accuracy of the results, (2) the contradictions observed, and also to produce reliable fundamental data for a variety of calcium silica based vanadium melts. This data is applicable to understanding of vanadium behavior in iron and steel making slags.

2. Experimental procedure

50 g of master melts were prepared from analytical grade CaO, MgO, Al_2O_3 , SiO_2 and V_2O_5 . All reagents were dried at $120^\circ C$ for 24 hrs, then carefully weighed and mixed. These were melted in a platinum crucible at $1600^\circ C$, crushed in a tungsten mill and analysed by XRF. Compositions and identifications of slags are given in Table I. The time to approach equilibration time was determined in a separate kinetic study.

A molybdenum wound electric resistance tube furnace was used for the equilibrium experiments (Fig. 2).

TABLE I Composition of slag samples

S. no.	CaO/SiO ₂ (molar ratio)	V ₂ O ₅ (mol%)	Al ₂ O ₃ (wt%)	MgO (wt%)
A	0.7	5	—	—
B	0.9	5	—	—
C	1.23	5	—	—
D	0.7	1	—	—
E	0.9	1	—	—
F	1.21	3	—	—
G	1.23	5	3.22	—
H	1.22	5	5.44	—
I	1.22	5	7.87	—
J	1.57	5	—	3.50
K	1.51	5	—	4.87

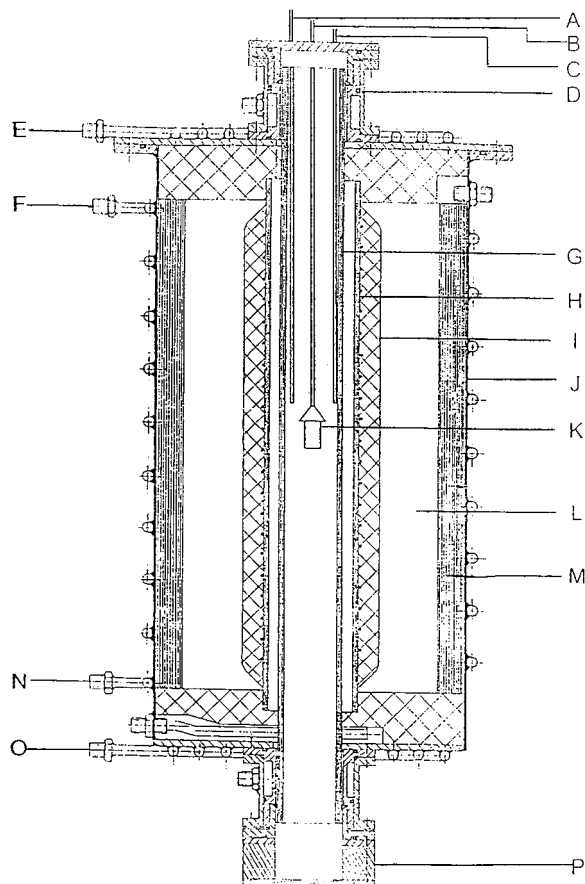


Figure 2 Vertical section of the molybdenum wound electric furnace: (A) To control thermocouple, (B) gas delivery tube, (C) to second thermocouple, (D) brass fittings, (E) water outlet, (F) gas outlet, (G) alumina reaction tube, (H) alumina outer tube, (I) heating element, (J) copper drum, (K) crucible, (L) alumina filling, (M) insulating wool, (N) gas inlet, (O) water inlet, and (P) quenching chamber.

Temperature of the furnace was controlled by an Eurotherm temperature controller ($\pm 5^\circ C$). 1–2 g of samples were placed in platinum crucible and equilibrated at $1600^\circ C$ in air and over a range of oxygen partial pressures (10^{-2} – 10^{-9} atm.). The samples were then quenched in the bottom water-cooled quenching chamber in the same gaseous atmosphere. Ar, CO, CO_2 and Ar- O_2 gas mixtures were used for the preparation of various compositions using precalibrated mass flow controllers. The equilibrium studies were carried out for series of master slags (A-K in Table I) at $1600^\circ C$ in platinum crucibles. The composition variables investigated

were alumina and magnesia content and basicity ratios over the above mentioned range of oxygen partial pressures.

The combined EPR/chemical analysis method detailed elsewhere [3] was employed for all slags. A Varian E-line spectrometer operating in X band at 9.48 GHz was used for the analysis of vanadium (IV). All spectra were recorded over 2000G at room temperature on quenched slags. Details of EPR analysis are also given earlier [2, 3].

3. Results and discussion

3.1. Vanadium redox reaction and oxygen partial pressures

The two redox equilibria corresponding to V^{3+}/V^{4+} and V^{4+}/V^{5+} pairs followed the O-type redox reaction [3] over the experimental oxygen partial pressures and temperature (10^{-2} – 10^{-9} atm, 1600°C) with V_2O_5 (5 mol%), alumina (3–8 wt%) and magnesia (3–5 wt%) contents investigated. The redox ratios decreased with increase in oxygen pressure, which is in accordance with limited previous work on sodium and calcium vanadium silicates [4, 6]; since data on the iron free $\text{CaO-SiO}_2\text{-V}_2\text{O}_5$, $\text{CaO-SiO}_2\text{-Al}_2\text{O}_3\text{-V}_2\text{O}_5$ and $\text{CaO-MgO-SiO}_2\text{-V}_2\text{O}_5$ slags are not available from the literature under the experimental conditions investigated here. Our previous work on soda slags [2, 3], is also in accordance with the findings for calcium silicate based slags, although the soda slags were mostly acidic ($\text{Na}_2\text{O/SiO}_2$: 0.5).

Generally the two redox pairs coexisted at oxygen potentials, 10^{-4} – 10^{-6} atm. This region is readily observed in Fig. 3a and b where the fractions of the three vanadium species are plotted at different oxygen pressures for $\text{CaO-SiO}_2\text{-V}_2\text{O}_5$ system (slags B and C, Table I). The oxygen pressure region for coexistence of two redox pairs was expanded with an increase in basicity (B: 0.9 to C: 1.23), as presented elsewhere [6].

3.2. Effect of basicity on vanadium redox equilibria

To find the effect of change in slag basicity, redox ratios (V^{3+}/V^{4+}) of slags B and C ($\text{CaO-SiO}_2\text{-V}_2\text{O}_5$ system) are compared in Fig. 4a, which reveals that the ratios decreased with increasing basicity (0.9 to 1.23). These plots indicate a good linearity. The section of oxygen partial pressures where V^{4+} and V^{5+} ions exist, was also extended from 10^{-4} atm at a basicity: 0.9, to 10^{-6} atm, by increasing the basicity to 1.23 [10].

Fig. 4b presents a plot of (V^{4+}/V^{5+}) ratios versus CaO/SiO_2 (molar ratio) at $p\text{O}_2$ 10^{-2} atm for slags B, C and F-K (Table I). It indicates a decrease in the redox ratios with increasing CaO/SiO_2 ratio and following linear equation was obtained incorporating all these slags.

$$\log \frac{V^{4+}}{V^{5+}} = -1.413 \frac{\text{CaO}}{\text{SiO}_2} - 1.386 \quad R^2 = 0.718 \quad (4)$$

It is evident from the results that an increase in ba-

sicity stabilizes the proportion of vanadium in higher oxidation states in the slags investigated, hence vanadium follows an O-type redox reaction [18–20], which agrees with our previous conclusions on sodium silicates [2].

A study made by Tsukihashi *et al.* [5] on $\text{CaO-CaF}_2\text{-SiO}_2$ slag (VO_x 3%) at 1300°C to determine the effect of addition of Na_2O addition on vanadium valencies during the hot metal treatment reveals that at a $p\text{O}_2$: 10^{-18} atm, the V^{4+}/V^{5+} pair was present in the melt whereas none of the present slags (A-K, Table I) contains this pair even at a higher oxygen pressure (i.e., 10^{-9} atm) at 1600°C . Their observation may be attributed to the presence of the several transition metals and traces of iron metal, affecting the true valency of vanadium in their slags.

Also, the addition of soda increased the valency of vanadium in the CaF_2 slags which supports the present findings, despite the difference in melt composition, that an increase in the oxygen ion activity ($a_{\text{O}^{2-}}$) increased the vanadium oxidation states. In addition, the increase in the vanadium distribution ratio between the slag and the hot metal increased by an order of magnitude on adding 2 wt% soda in the CaF_2 slag investigated by Tsukihashi *et al.* which supports the earlier observations indicating the effect of increasing basicity in soda slags [1, 2, 9, 10].

A comparison of x , the non stoichiometry of vanadium oxide, between slags B and C (V_2O_5 : 5 mol%, basicity: 0.9, 1.23 respectively) and $\text{CaO-SiO}_2\text{-V}_2\text{O}_5$ slags melted at 1600°C over $p\text{O}_2$ range: 10^{-1} – 10^{-8} atm from Mittelstadt and Schwerdtfeger [4] is presented in Fig. 5. Here the tabulated data at basicity ratios: 1.0 and 1.36 ($V_2O_5 \sim 10$ mol%) obtained from chemical analysis [4] is plotted. It indicates that the “ x ” remained lower for slags B and C, compared to those of Mittelstadt and Schwerdtfeger, particularly at higher oxygen partial pressures ($\geq 10^{-5}$ atm). Though this may be attributed to the experimental error and difference in analytical techniques used, as our results show less uncertainties by employment of newly developed analytical technique. Nevertheless low basicity (0.9, 1.23) reduces the “ x ” to smaller values compared to that of 1.0 and 1.36 respectively, as expected.

3.3. Dependence of valance states of vanadium on alumina content

Although the alumina contents investigated produced a slight increase in the redox ratios (V^{3+}/V^{4+}) by enhancing the acidity of the melts, clear trends have not been observed. This is illustrated in Fig. 6 where $\log(V^{3+}/V^{4+})$ is plotted against $\log p\text{O}_2$ at different alumina levels for the slags G-I ($\text{CaO-SiO}_2\text{-Al}_2\text{O}_3\text{-V}_2\text{O}_5$ system) and the alumina free slag C ($\text{CaO-SiO}_2\text{-V}_2\text{O}_5$ system) (Table I). A slight increase in the redox ratios is obvious when the alumina concentration was changed from 3.22 to 5.44% at a basicity ratio ~ 1.3 . Alumina is generally considered amphoteric. Since the concentration of alumina investigated was low, it may be insufficient to produce a significant change in the redox ratios. The authors have also previously observed

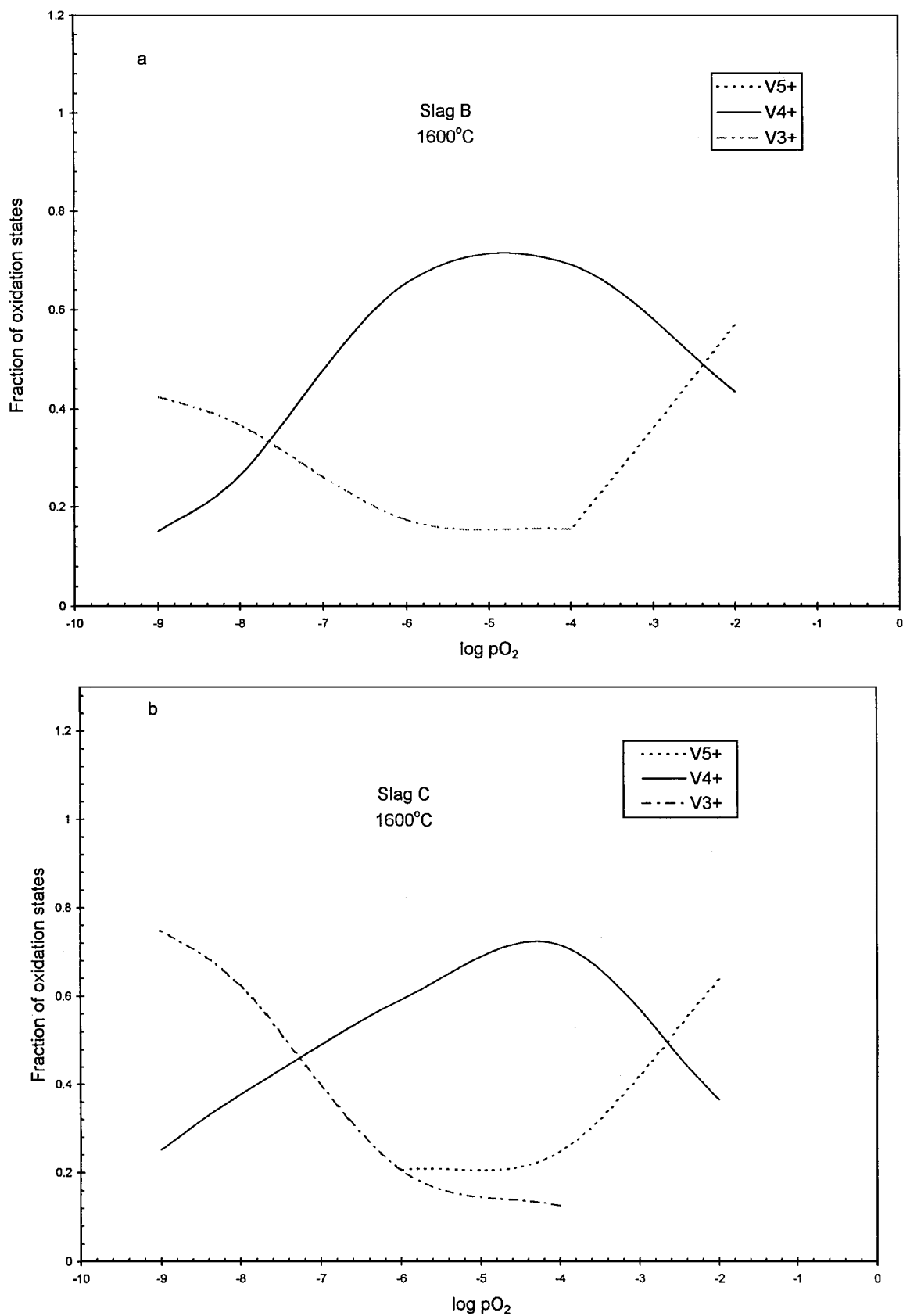


Figure 3 Dependence of fraction of redox species of vanadium (CaO-SiO₂-V₂O₅ system, 1600°C) on oxygen partial pressures at CaO/SiO₂: (a) 0.9 (slag B) and (b) 1.23 (slag C) See Table I for details.

that the addition of different alumina contents had no effect on the oxygen partial pressure region where two redox pairs coexist at measurable concentrations [3].

3.4. Effect of magnesia on vanadium oxidation states

Magnesia, a basic oxide, acts as a network modifier and increases the activity of free O²⁻ ions in

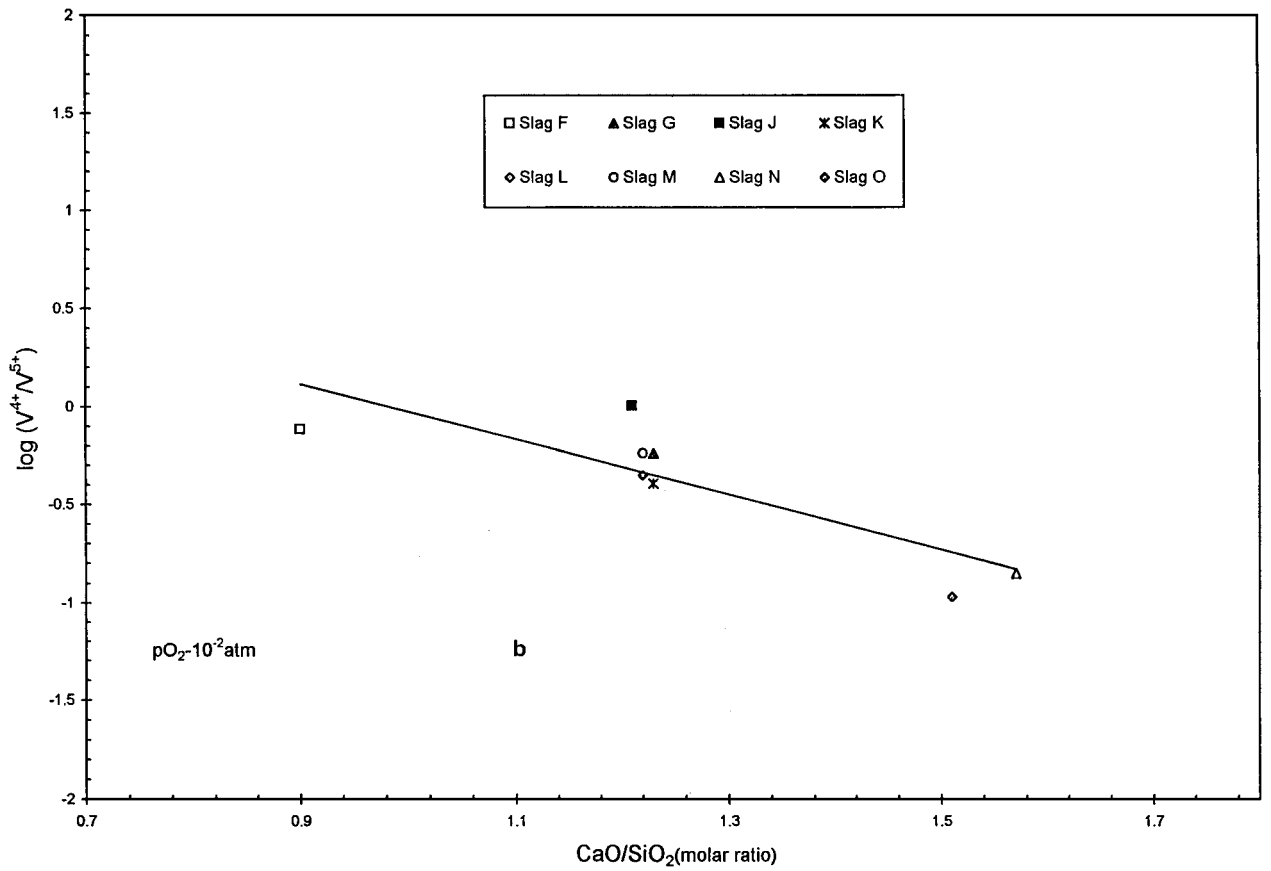
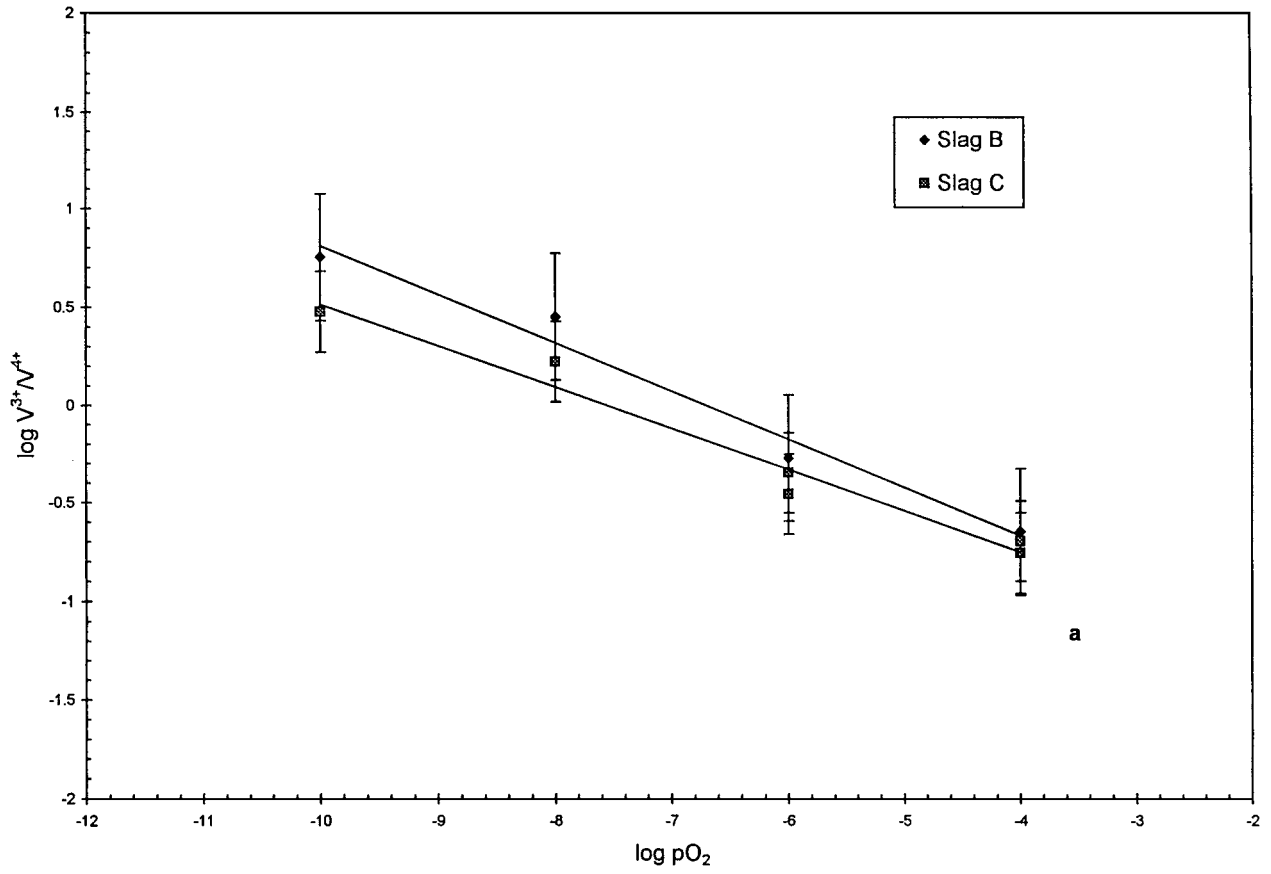


Figure 4 (a) Change in V³⁺/V⁴⁺ ratios (CaO-SiO₂-V₂O₅ system, 1600°C) with log pO₂ at different basicity ratios (slag B: 0.9 & slag C: 1.23) and (b) Change in V⁴⁺/V⁵⁺ ratios as a function of CaO/SiO₂ ratio for slags B,C, E-K, See Table I for details.

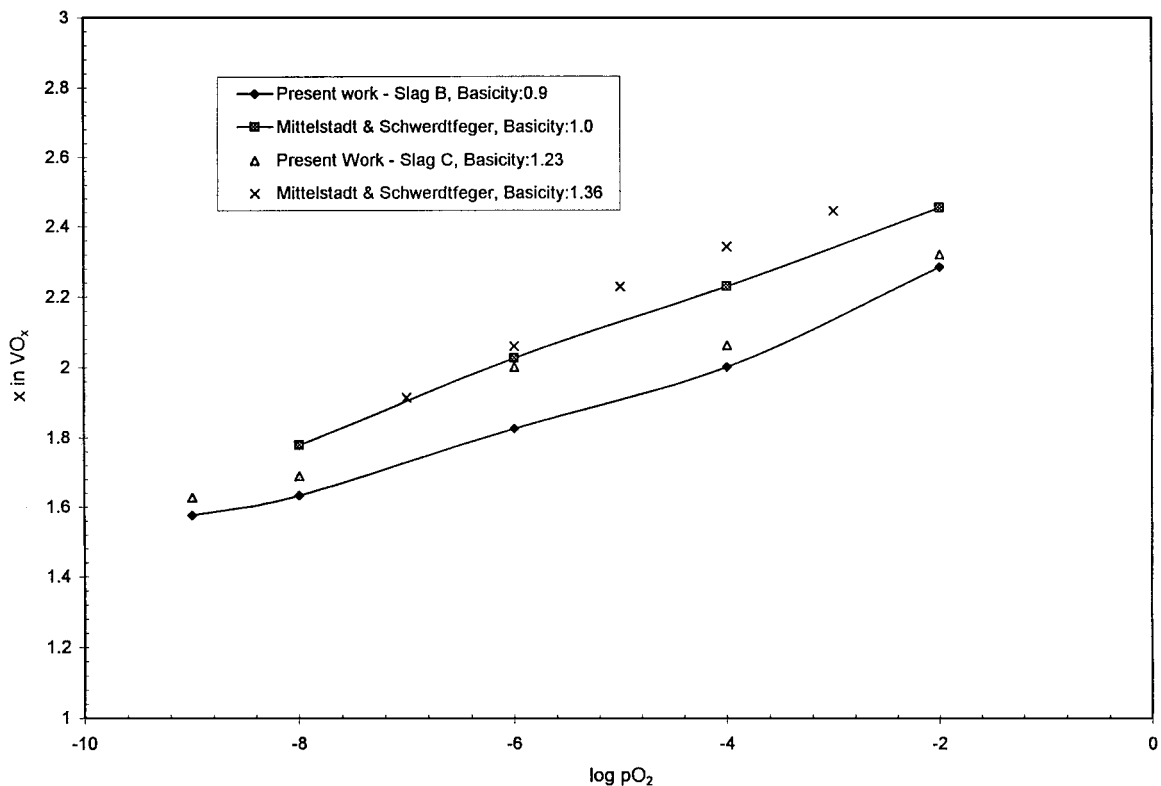


Figure 5 Comparison of overall oxidation state, x in VO_x , in $\text{CaO-SiO}_2\text{-V}_2\text{O}_5$ system as a function of oxygen partial pressures at basicity 0.9 & 1.23 ($\text{V}_2\text{O}_5 = 5$ mol%) with those of Mittelstadt and Schwerdtfeger [4] at basicity 1.0 & 1.36 ($\text{V}_2\text{O}_5 = 10$ mol%) at 1600°C .

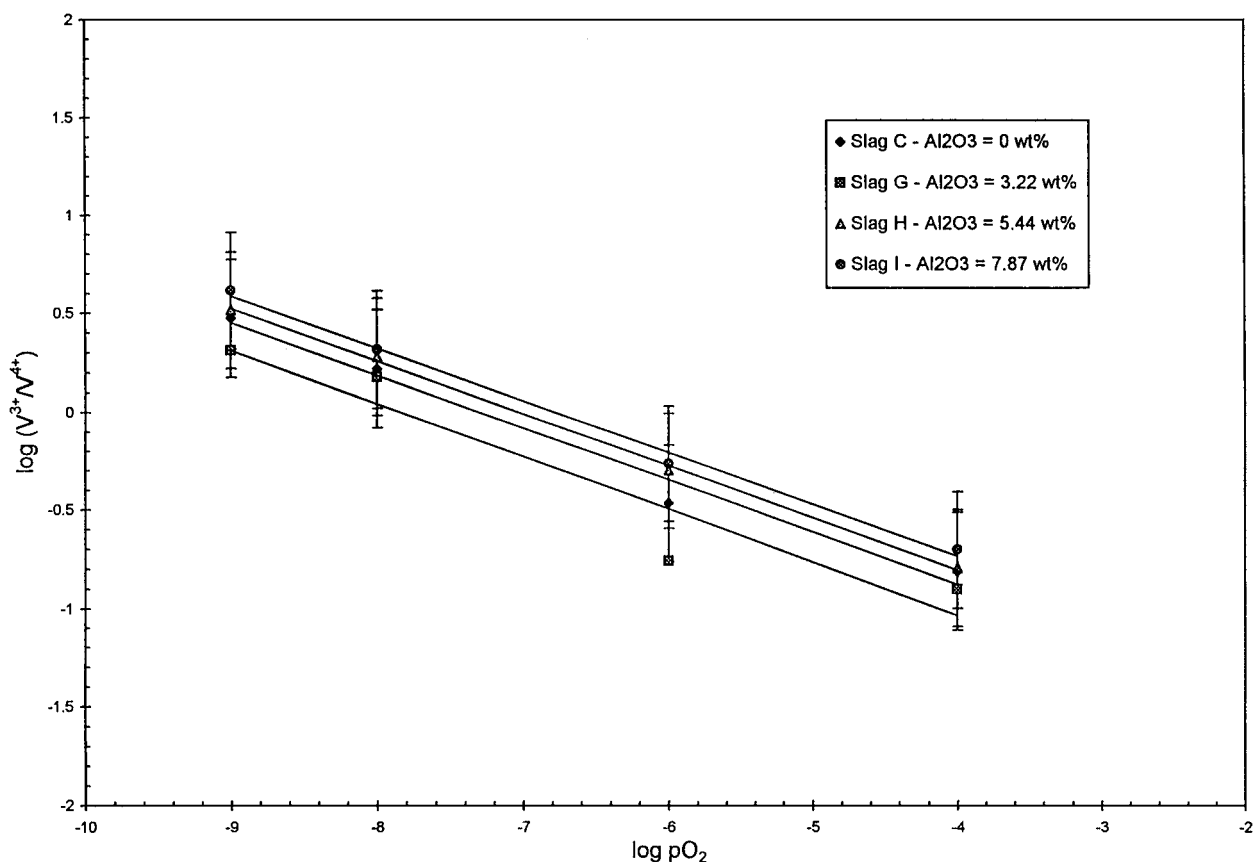


Figure 6 Change in redox ratios ($\text{V}^{3+}/\text{V}^{4+}$) ($\text{CaO-SiO}_2\text{-Al}_2\text{O}_3\text{-V}_2\text{O}_5$ system) with respect to oxygen pressures at different alumina levels (1600°C).

the melt. As expected, the ratio of the redox species ($\text{V}^{4+}/\text{V}^{5+}$) between 10^{-2} – 10^{-6} atm decreased sharply with the 3.5 wt% addition of MgO ($\text{CaO-MgO-SiO}_2\text{-V}_2\text{O}_5$ system) (Fig. 7). The reduction in the valency ratio was less with a further addition of MgO

to 4.87 wt%. This trend generally agrees with previous work [11]. However it is surprising that addition of magnesia caused the overlapping region of the three valence states to diminish. Within the experimental error, there was no oxygen potential

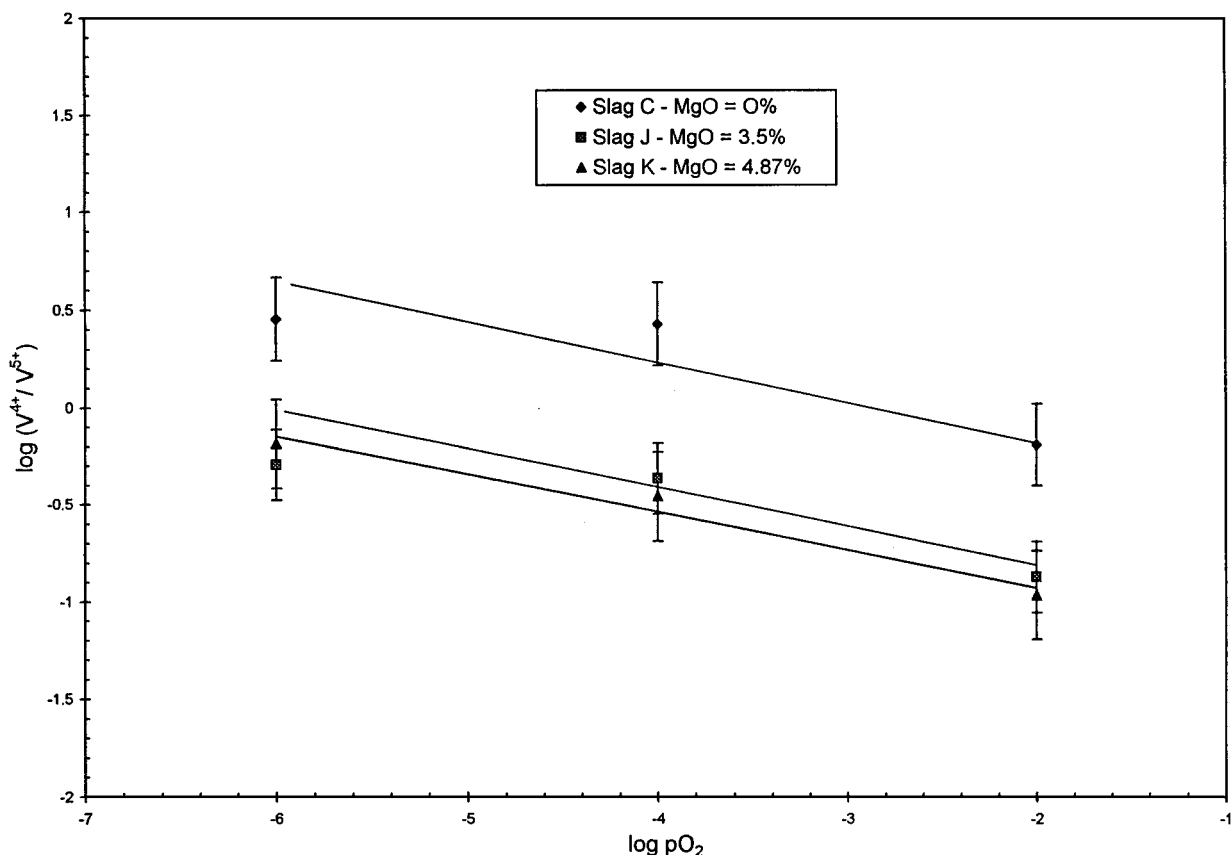


Figure 7 Effect of MgO addition on redox ratios (V^{4+}/V^{5+}) over different oxygen pressures (CaO-MgO-SiO₂-V₂O₅ system) (1600°C).

at which all the valencies coexisted in these slags [3].

Fig. 8 presents variation of vanadium valency ratios (V^{4+}/V^{5+}) versus (CaO + MgO)/SiO₂ molar ratios for slag C (CaO-SiO₂-V₂O₅ system), J and K (CaO-MgO-SiO₂-V₂O₅ system) at an oxygen potential of 10⁻⁴ atm. and those of CaO-MgO-FeO-SiO₂ slags studied by Inoue and Suito [11] equilibrated with liquid iron ($V \sim 1.5$ wt%). The data points are taken from the tables, at an oxygen pressure of 10⁻⁹ atm at 1600°C. It is difficult to compare these iron bearing slags with the present work due to the difference in composition and unavailability of the data over various oxygen potentials. However the both sets of data show a decrease in the V^{4+}/V^{5+} ratio with increasing MgO content and/or the basicity ratio. In Inoue and Suito's work, FeO has acted as a basic oxide and contributed towards stabilization of V⁵⁺; although the presence of V⁴⁺/V⁵⁺ pair at the reduced pressure (10⁻⁹ atm) disagrees with the current work, where none of the slags contained this redox pair at this oxygen potential.

Other magnesia bearing iron silicate slags with vanadium (wt%) ~ 1.7 -2.3 at 1300°C have been studied by Werme [15, 16] and an overall valency as V³⁺ was present at pO₂ $\sim 10^{-12}$ -10⁻¹⁵ atm. It supports the current results where the V⁴⁺/V⁵⁺ pair was present under lower oxygen potentials (at 10⁻⁸ and 10⁻⁹ atm). However other experimental data is unavailable over the present oxygen pressure range for comparison. It should be noted that addition of basic oxides (CaO, MgO, Na₂O) changed the activity of FeO and the equilibrium oxygen potential in Werme's iron bearing melts,

therefore vanadium valency did not increase with an increase in basicity.

3.5. Effect of V₂O₅ content on vanadium valencies

The redox ratios V³⁺/V⁴⁺ and V⁴⁺/V⁵⁺ for slags F and C which have almost identical basicity (CaO-SiO₂-V₂O₅ system) containing 3 and 5 mol% V₂O₅ respectively are plotted in Fig. 9. From a close examination, it appears that the redox ratios V⁴⁺/V⁵⁺ did not indicate clear trends. The ratios V³⁺/V⁴⁺ are slightly lower for slag F. Therefore the redox equilibria are independent of the change in V₂O₅ content studied.

It has been found earlier in glasses [22, 23] that the redox ratios V⁵⁺/V⁴⁺ increased with the addition of this oxide, which indicates its basic character or network breaking or depolymerising ability. In contrast, Mittelstadt and Schwerdtfeger [4] have reported a decrease in vanadium oxidation state with a decrease in Na₂O/V₂O₅ molar ratios (1.0 to 0.2) in Na₂O-V₂O₅ melts, indicating V₂O₅ as a network former. The discrepancy may be attributed to the differences in the oxygen pressure and possibly the glass composition studied, since all glass investigations reported in the literature were carried out under highly oxidized conditions i.e., in oxygen or air, while those of Mittelstadt and Schwerdtfeger were over the oxygen pressures range of 10⁻³ and 10⁻⁹-10⁻¹⁶ atm. The overall oxidation state in Mittelstadt and Schwerdtfeger's work corresponded to V⁵⁺ at 10⁻³ atm at different V₂O₅

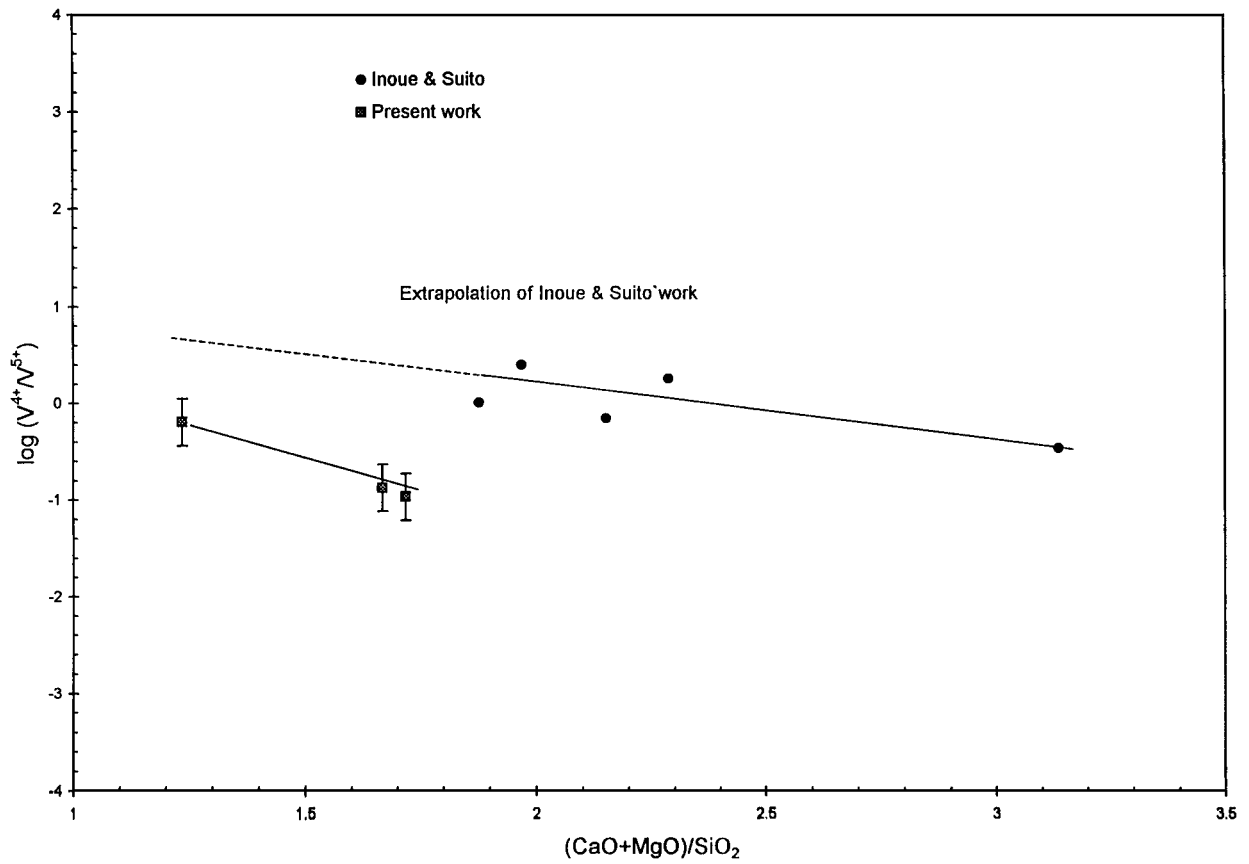


Figure 8 Comparison of redox ratios of vanadium between present work (slags C (CaO-SiO₂-V₂O₅), J & K (CaO-MgO-SiO₂-V₂O₅ system) and those of Inoue & Suito [11] (1600°C). See Table I for details.

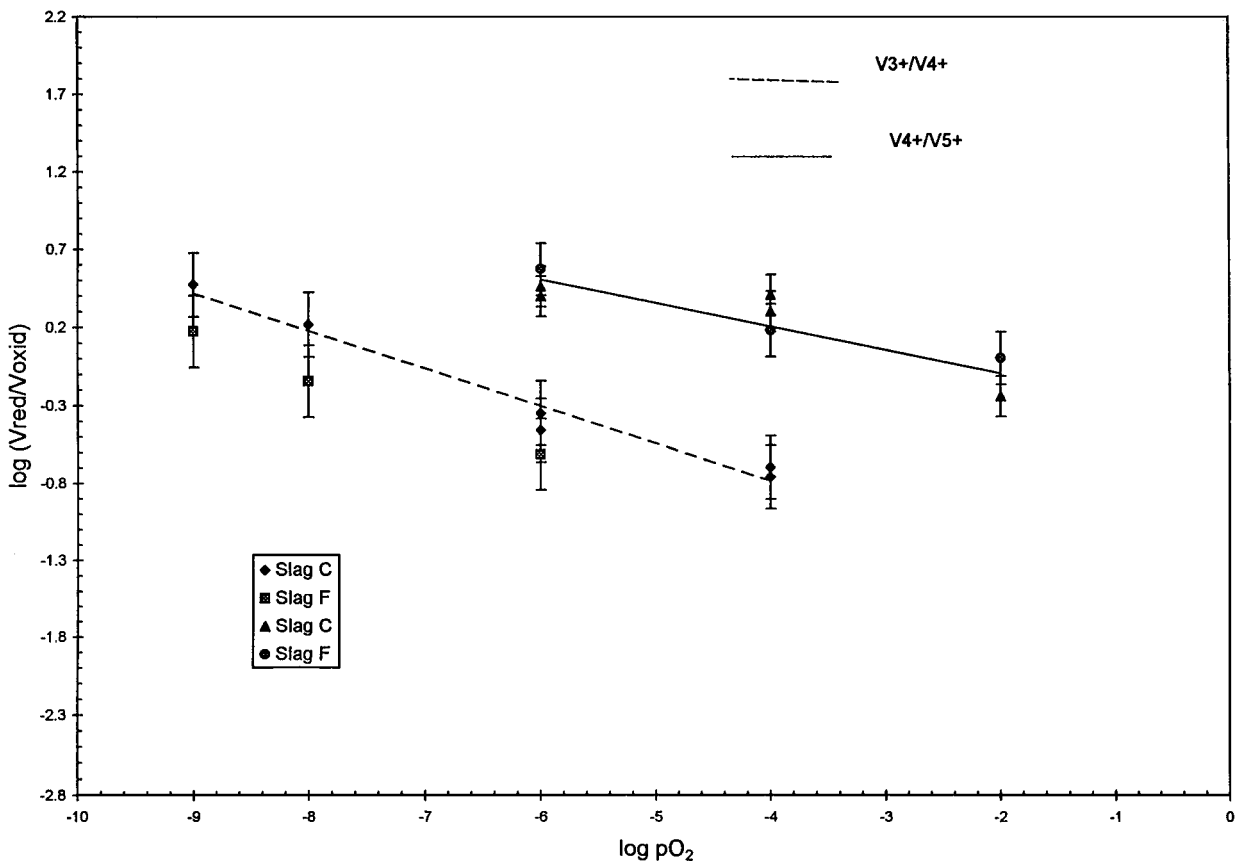


Figure 9 Effect of variation of total vanadium content on vanadium redox ratios in CaO-SiO₂-V₂O₅ system (V₂O₅ = 3 mol% for slag F & 5 mol% for slag C). See Table I for details.

contents. Below 10^{-9} atm, it decreased with an increase in V_2O_5 content. Hence the effect of reduced oxygen pressure on the oxidation state, cannot be disregarded. Therefore this oxide acts as a network former. In the present investigation, with a maximum of 5 mol% investigated, V_2O_5 acted as a neutral oxide, when compared to the concentrations > 10 mol% as found in other investigations.

4. Conclusions

The newly developed method, which enables quantitative determination of the three oxidation states of vanadium, was successfully evaluated and applied to calcium silicates and complex melts. In calcium silicates, the two redox equilibria corresponding to the V^{3+}/V^{4+} and the V^{4+}/V^{5+} pairs followed O-type redox reaction over oxygen partial pressures 10^{-2} – 10^{-9} atm at 1600°C with V_2O_5 (1–5 mol%), alumina (3–8 wt%) and magnesia (3–5 wt%) contents investigated. This result contradicts of previous workers [11, 24] who used both O and R-type redox expressions to describe the vanadium behavior. Generally the two redox pairs coexisted in measurable concentration over oxygen potentials 10^{-4} – 10^{-6} atm.

In Al_2O_3 -CaO- SiO_2 - V_2O_5 slags, there was a slight increase in the redox ratios, when alumina quantity was changed from 3.22 to 5.44% at a basicity ratio ~ 1.3 . However overall, there is no obvious change in the average vanadium valency for melts containing between 3 and 8 wt% alumina.

In CaO-MgO- SiO_2 - V_2O_5 melts, the ratio of redox species (V^{4+}/V^{5+}) decreased sharply with the addition of 3.5 wt% MgO over the oxygen partial pressure range 10^{-2} – 10^{-6} atm at 1600°C. Although the same trend was observed when the MgO content was further increased to $\sim 5\%$, the reduction in the valency ratio was small. This trend generally agrees with previous work [4]. Within the experimental error, there was no oxygen potential at which all the valencies coexisted in these slags.

The redox ratios V^{3+}/V^{4+} and V^{4+}/V^{5+} (CaO- SiO_2 - V_2O_5 system) did not indicate clear trends with a change in V_2O_5 content from 3 to 5 mol%. Therefore the redox equilibria and the overall valency of vanadium are independent of the change in V_2O_5 content studied.

Acknowledgment

The authors gratefully acknowledge the financial support for this project from BHP Research, Center for Metallurgy and Resource Processing, Newcastle, Australia and access to EPR facilities from School of Physics, University of New South Wales, Sydney, Australia.

References

1. H. FARAH, M. P. BRUNGS, D. J. MILLER and G. R. BELTON, *Phy. Chem. Glasses* **39** (1998) 318.
2. H. CHAUDARY, M. P. BRUNGS, D. M. MILLER and G. R. BELTON, in Proceedings of the 5th International Conference on Molten Slags, Salts and Fluxes, Sydney, January 1997 (ISS, Warrendale, 1997) p. 493.
3. H. FARAH, Ph.D. Dissertation, University of New South Wales, Australia, 1999.
4. R. MITTELSTADT and K. SCHWERDTFEGGER, *Met. Trans. B* **21** (1990) 111.
5. F. TSUKIHASHI, T. TAGAYA and N. SANO, *Trans. I.S.I.J.* **28** (1988) 164.
6. W. D. JOHNSTON, *J. Amer. Ceram. Soc.* **48** (1965) 184.
7. H. D. SCHREIBER, *J. Non-Cryst. Solids* **42** (1980) 75.
8. *Idem.*, "Advances in Materials Characterization" (Plenum, New York, 1983) p. 647.
9. H. FARAH, *J. Mater. Sci.* **38** (2003) 727.
10. H. FARAH and M. P. BRUNGS, *J. Mater. Chem.* (2002).
11. R. INOUE and H. SUITO, *Trans. I.S.I.J.* **22** (1982) 705.
12. R. SELIN, Ph.D thesis, The Royal Institute of Technology, Stockholm, 1987.
13. *Idem.*, in Proceedings of International Conference on Molten Slags and Fluxes (Inst. of Metals, Glasgow, 1989) p. 317.
14. A. WERME, *Steel Research* **59** (1988) 6.
15. A. WERME and C. ASTRON, *Scan. J. Met.* **15** (1986) 273.
16. A. WERME, Ph.D thesis, The Royal Institute of Technology, Stockholm, 1987.
17. SCHLACKENATLAS "Verlag Stahleisen M.B.H., Dusseldorf, 1981 Vol. 1, p. 2.
18. H. D. SCHREIBER, *J. Non-Cryst. Solids* **84** (1986) 129.
19. S. WRIGHT and S. JAHANSHAH, (Apcche-Chemeca, Melbourne, 1993) Vol. 2, p. 359.
20. S. B. HOLMQUIST, *J. Amer. Ceram. Soc.* **49** (1965) 228.
21. E. T. TURKDOGAN, "Physical Chemistry of High Temperature Technology" (Academic Press, New York, 1980) p. 145.
22. E. J. FRIEABLE, L. K. WILSON and D. L. KINSER, *J. Amer. Ceram. Soc.* **55** (1972) 164.
23. S. GUPTA, N. KHANIJO and A. MANSINGH, *J. Non-Cryst. Solids* **181** (1995) 58.
24. M. NAGANO, A. KATO, I. MOCHIDA and T. SEIYAMA, *J. Ceram. Soc. Japan* **78** (1970) 401.

Received 7 August 2002

and accepted 26 February 2003